

Composite Materials for Wind Blades: Current Performance and Future Directions



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- 1. PPG Wind Energy
- 2. Evolution of wind blade materials
- 3. The current state –performance review
- 4. Alternatives for stronger, stiffer blades
- 5. The future state long term goals and new developments



PPG Wind Energy

1. PPG Wind Energy

- Offering a multitude of products for wind turbines
 - Fiber glass for blades, nacelles
 - Coatings for blades, towers
- World leader in fiber glass
 - Established in wind energy for 15+ years
 - Production and sales from 3 major continents
 - Hybon® 2002/2001 recognized product in wind energy blades
 - Specified in blades from most major manufacturers around the world
 - Continuing to develop new products that will enhance wind energy production for the future











PPG Wind Energy Fiber Glass Product History

1. PPG Wind Energy



- Specified and used at most wind turbine companies
- Designed for multiple resin compatibility

Hybon® 2026

- Multiple resin compatibility
- Enhanced processing characteristics
- Improved strength and fatigue life

	Tensile Strength		Short Beam Shear Strength	FWF
Units	MPa	MPa	MPa	%
Method	ISO 527-5	ISO 14125	ISO 14130	
Sample Prep	А	А	В	
Hybon® 2002	1107	1221	64	74.8
Hybon® 2026	1148	1339	67	75.6

- A Unidirectional infused panels, Hexion RIM 135 epoxy
- B Filament wound cylinders per ASTM D 2291



Fiber/Fabric Processing

Blade Performance Nano scale to Mega Watt

Infusion, fatigue, weight

1. PPG Wind Energy



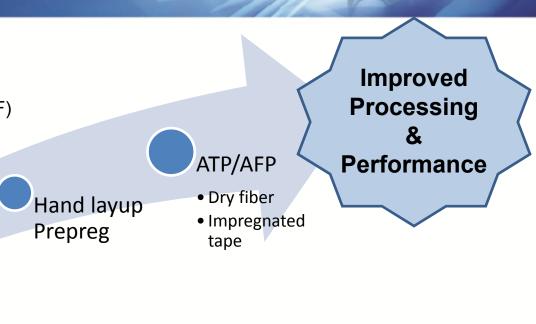


Evolution of wind turbine blade production

2. Evolution of wind blade materials

Input materials

- Core materials (balsa, PVC, PU, etc.)
- Skin materials (multiaxial fabrics NCF)
- Spar materials (UD, multiaxial fabrics NCF)
- · Root materials (roving, multiaxial fabrics)
- Resin systems (DGEBA, VE, PE, ...)



Vacuum Infusion

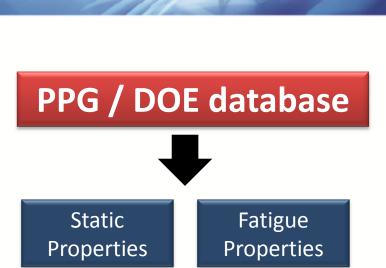
Wet layup
Wet winding





Performance review

- SNL/MSU/DOE database
- Optidat Database
- PPG internal test data
- Other public information







Material forms



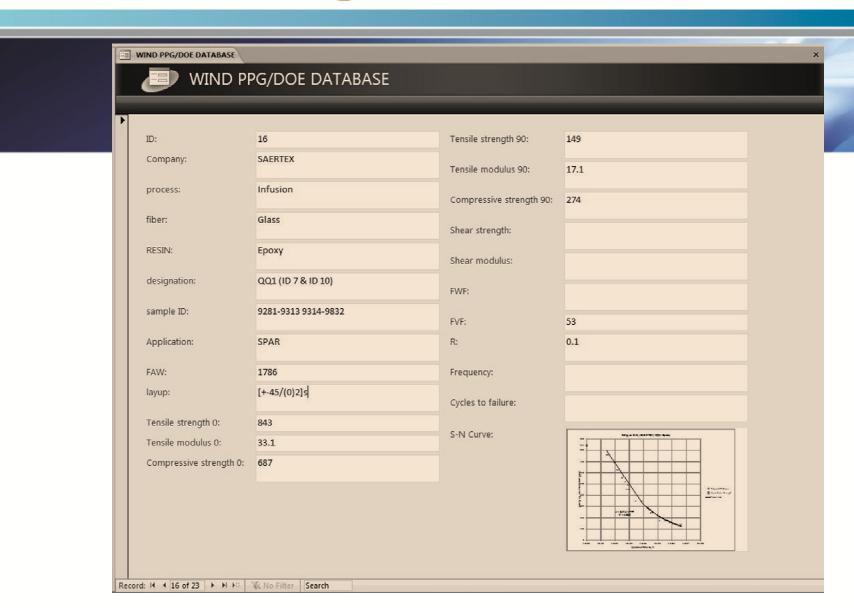
- UD, Biax
- Infusion grade materials
 - UD, Biax, Triax

APPLICATION/ REINFORCEMENT	UD	BIAX 0/90 – 45	TRIAX	ROVING
WEB				
SPARCAP				
SKIN				
ROOT				





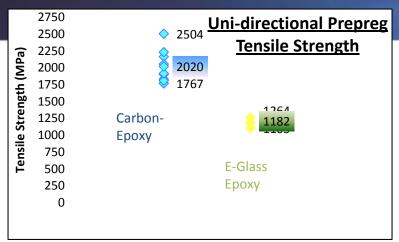
Electronic Database

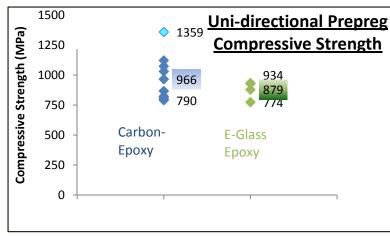


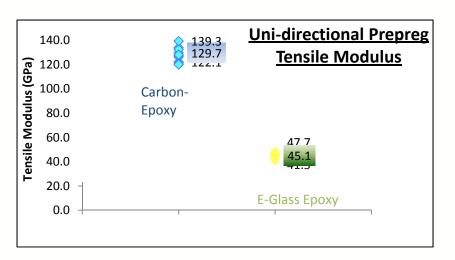




UD Prepreg Static Properties



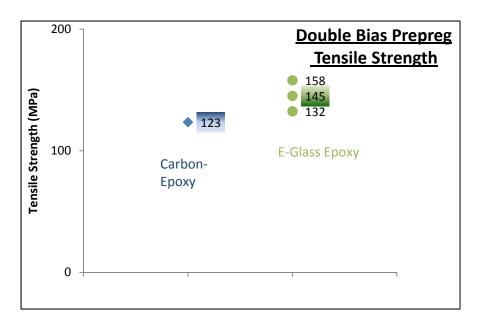


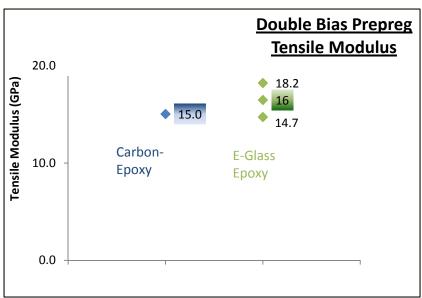






Double bias Prepreg Static Properties



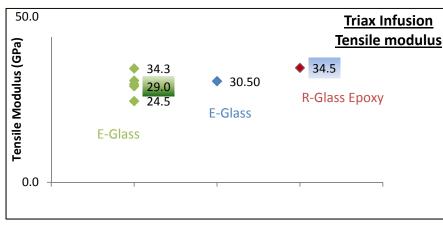


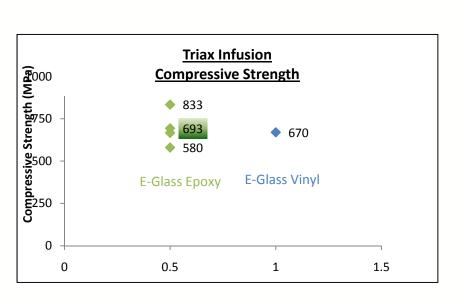




Triaxial Infusion Static Properties









How to drive performance?

4. Alternatives for stronger, stiffer blades



2. <u>Material performance enhancements (strength and/or stiffness)</u>

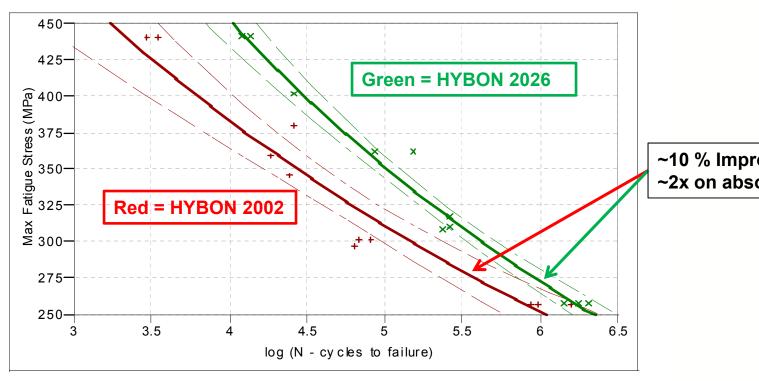
- 1. Sizing Chemistry (strength)
- 2. Fiber Composition (strength + stiffness)
- 3. Fiber Volume Fraction (strength + stiffness)
- 4. Defect reduction/prevention (strength*)

^{*}at component level



Sizing Chemistry

Alternatives for stronger, stiffer blades: 4. Sizing Chemistry

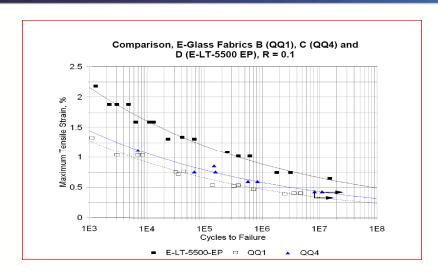


~10 % Improvement ~2x on absolute scale



Sizing Chemistry

4. Alternatives for stronger, stiffer blades: Sizing Chemistry

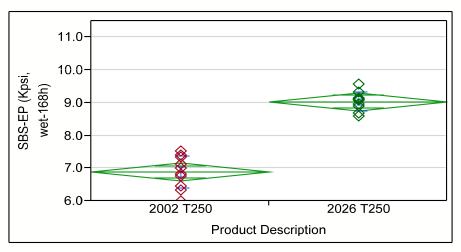


Resin: EP = EPON 826 Method: SBS = ASTM D2344

All testing on 1984 TEX (250 Yield) rovings

Montana State results

- Vectorply E-LT 5500 using Hybon® 2026
 4400TEX input in zero direction
- Supports value of Hybon® 2026





Fiber Volume Fraction

4. Alternatives for stronger, stiffer blades: Increase FVF



- Avenue for increasing spar cap stiffness (reduction in tip deflection)
- Achievable with existing materials

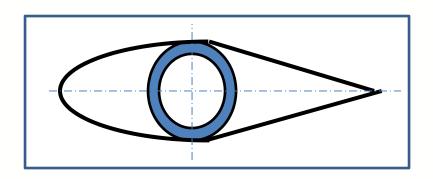
Disadvantages:

- Effect on long term performance of composite laminate (fatigue)?
- Increase in weight
- Difficulties in processing (dry spots)



Hypothetical case FVF

- Alternatives for stronger, stiffer blades: Increase FVF
- Circular cross section spar
- Parameters include
 - Outside Diameter (OD), Inside
 Diameter (ID)
 - Spar length (L)
 - Elastic Modulus of Fiber (Ef)
 - Fiber Volume Fraction (FVF)



OD = 0.6 m, ID = 0.55 m

L = 60 m

Ef = 79 GPa (Impregnated strand tensile)

FVF = 50%

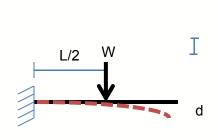
Modulus translation efficiency = 97%

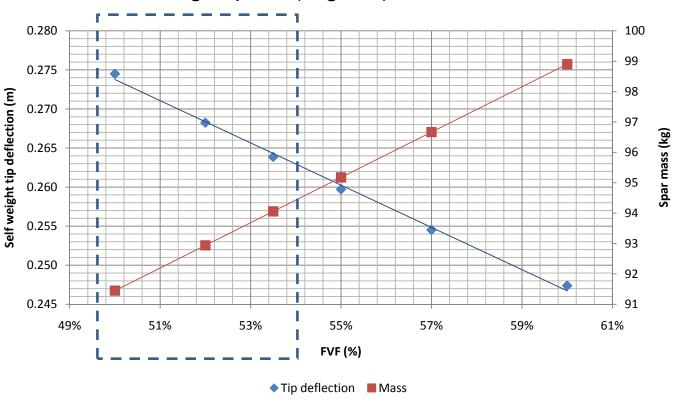


Effect of FVF on tip deflection of spar, self weight

4. Alternatives for stronger, stiffer blades: Increase FVF

Common design space (E-glass)



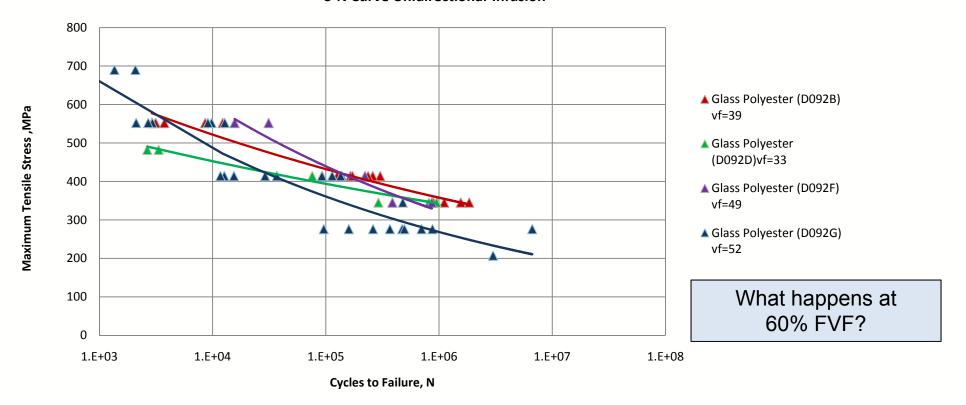




Effect of FVF on dynamic properties

4. Alternatives for stronger, stiffer blades: Increase FVF

S-N Curve Unidirectional-Infusion





Reinforcement Landscape - Fiber Properties

4. Alternatives for stronger, stiffer blades: Fiber Composition

Fiber Types	E glass	R glass	S glass	Carbon
Density (g/cm³)	2.55 – 2.64	2.55	2.46 - 2.49	1.7
Young's Modulus (GPa)	70 – 77	84-86	86 – 90	220
Pristine Strength (MPa)	3450 – 3790* 2800 **	4400* 3900 **	4590 – 4830	3800**
Failure Strain (%)	4.5 – 4.9		5.4 – 5.8	0.7

^{*}pristine

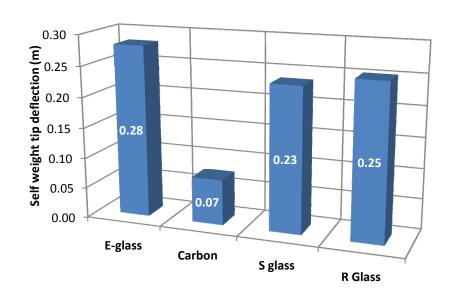
^{**}impregnated strand per ASTM D2343

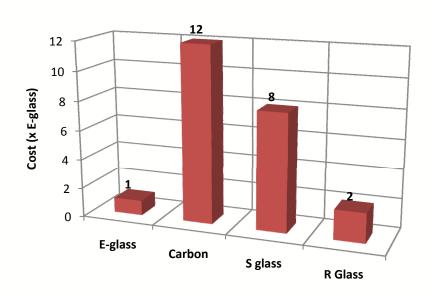


Edge deflection on spar model

4. Alternatives for stronger, stiffer blades: Fiber Composition

As Fiber Modulus Increases, deflection is reduced but cost per lb increases...

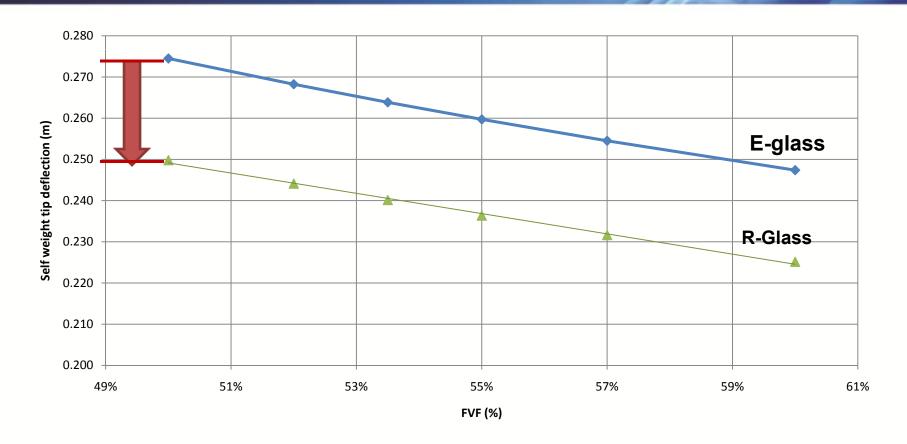






Composition shift E to R

4. Alternatives for stronger, stiffer blades: Fiber Composition





What is next?

5. The future state – long-term goals and new developments

- Faster, easier processing
 - Faster wet-out for liquid molding
 - Reduced probability of porosity in laminates
 - Reduced abrasion
- Defect reduction
 - Material forms adequate for FP/ATP (process driven)
 - Resin specific sizing technology (innovative film former chemistry)
 - Higher Tensile strength
 - Higher SBSS and strength retention
 - Improved fatigue performance







New material forms and process development

5. The future state – long-term goals and new developments

- ATL/FP grade materials
 - Equilibrium between performance and cost
 - Material tolerances
 - Paper requirements
 - Impregnation levels and slitting characteristics
 - Tack
 - In situ consolidation









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